



Pulverizer Plant O&M Aspects

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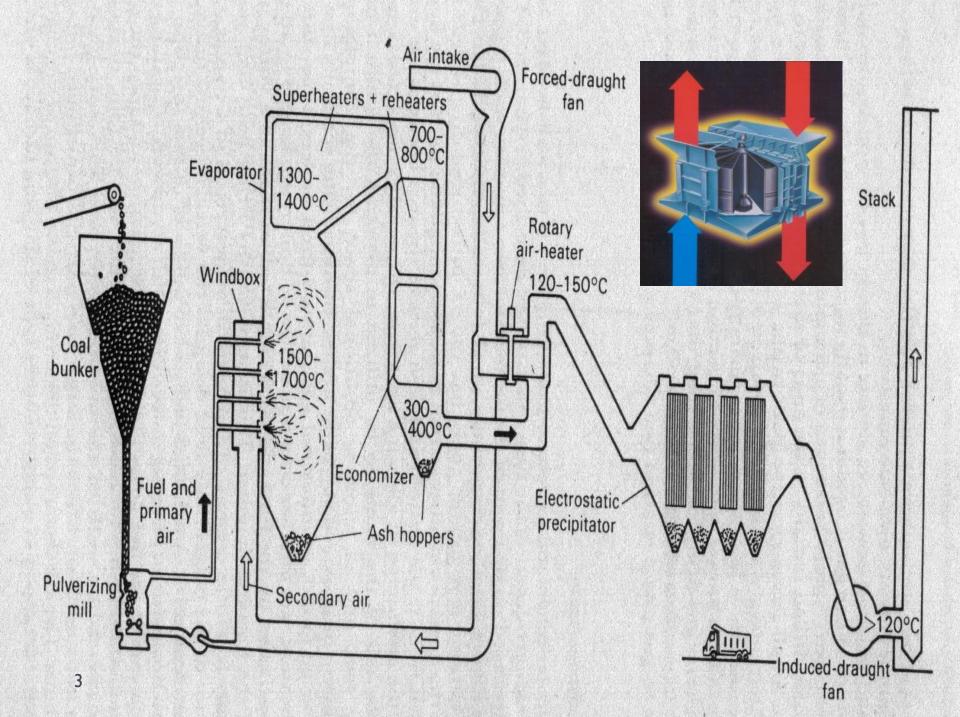
Contents



Mill operational issues

Constructional features and maintenance

Performance issues and case studies



The Three Ts & One S Practice

Technology	Time	Temperature	Turbulence	Size
Stoker	large	Medium	Low	Big
Pulverized	Short	High	Medium	Tiny
Cyclone	Short+	V High	High	Medium
Fluid Bed	Medium	Low	High	Medium

Size the Coal and Add the Air !!!

Coal – an organic complex polymer

Sequential events

- Devolatilization (Pyrolysis)
 - Heating causes its structure to decompose
 - Weaker chemical bonds break at lower temperatures
 - Stronger ones at higher temperatures
 - Volatile yield can be up to 50%
 greater than indicated by proximate analysis



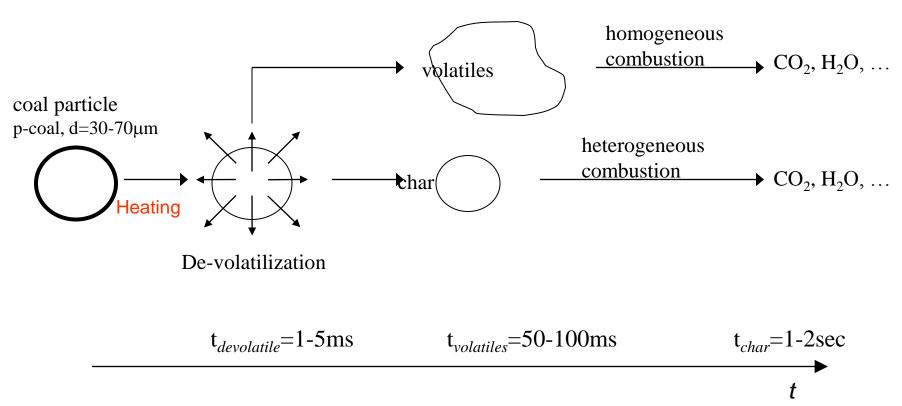


- Burning of volatile matters
 - Homogeneous gas phase reaction around the particle
- Char burning
 - Heterogeneous combustion
 - Occurs at the char surface and pore surfaces (porosity~0.7; surface area ~100 m²/g)
 - Guided through competing effects
 of heat and mass transfers to the
 char surface and chemical reaction



Char particle at the early stage of burning

Coal Combustion

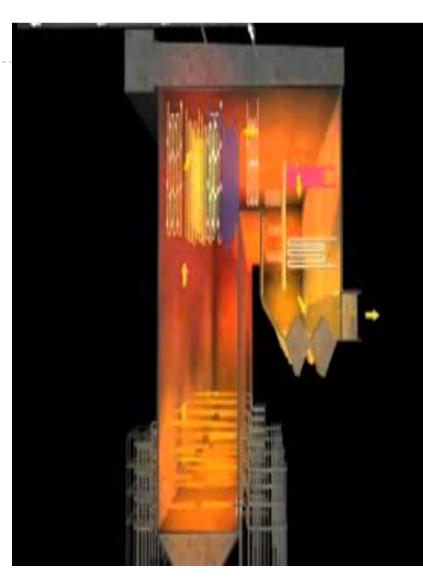


Temperature, Turbulence, **Time** and Size

VM, Fineness, Combustion & Residence Time

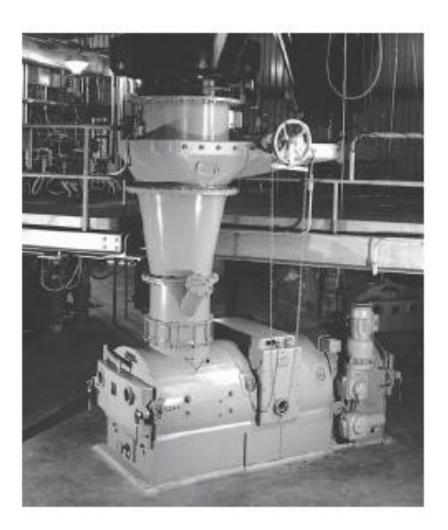
- Vol. combustion intensity, I_v is in the range 150-250 kW/m³.
- FEGT<IDT
- For a desired I_v, one can select t_r (~ 2 sec)
- The combustion time, t_c (~ 1 sec) <t_r by a significant margin.
- Low VM coal; more fineness required





Gravimetric Feeder

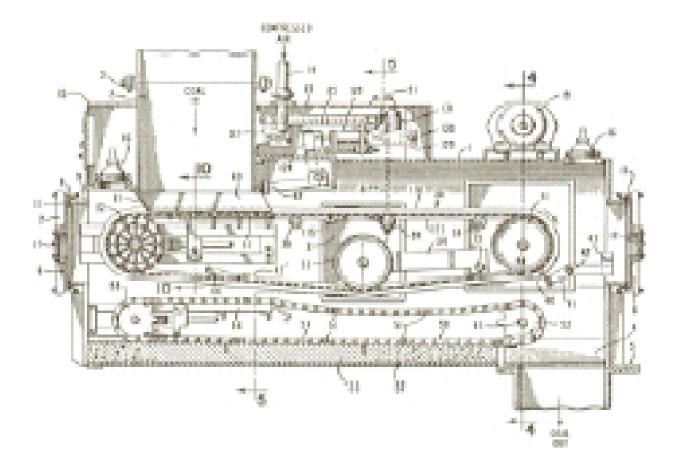




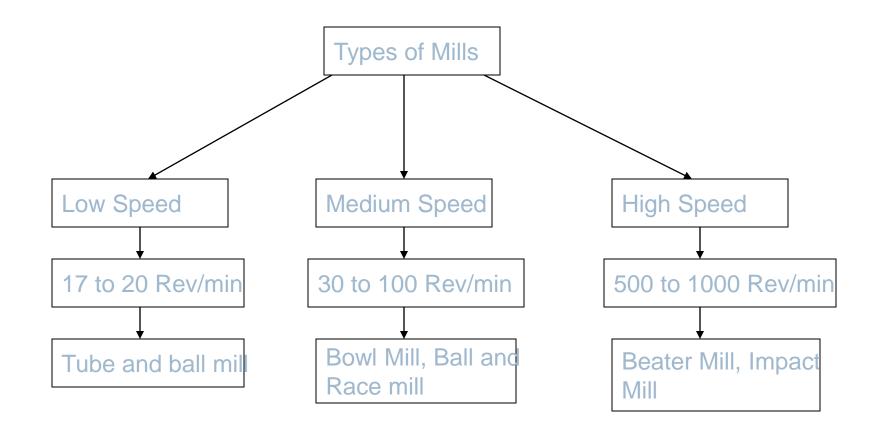
Gravimetric Coal feeder



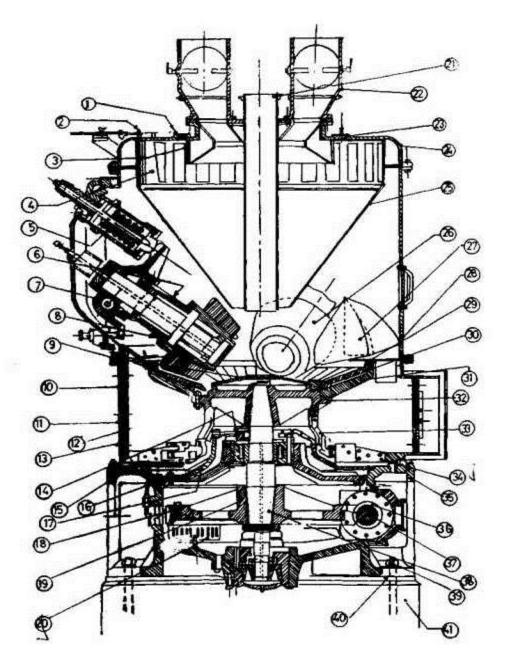
Internals of coal feeder



Classification-As per Speed



BOWL MILL



Model no.	Base capacity(T/Hr)
623XRP 703XRP 763XRP 803XRP 883XRP 903XRP 1003XRP	18.4 26.4 33.8 36.5 51.1 54.1 68.1
1043XRP	72.0

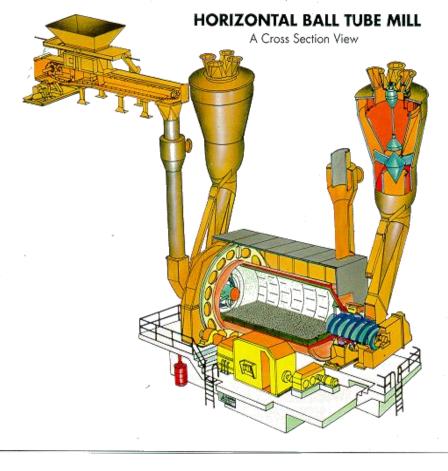
BASE CAPACITY(T/HR) AT HGI -55 Total Moisture-10% Fineness-70% THRU 200 MESH

Types of pulverisers

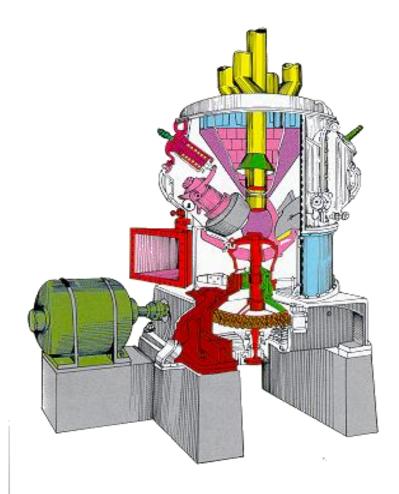
- Based on principles of particle size reduction
 - Impact
 - Attrition
 - Crushing
- Pulverisers use one, two or all the three principles.

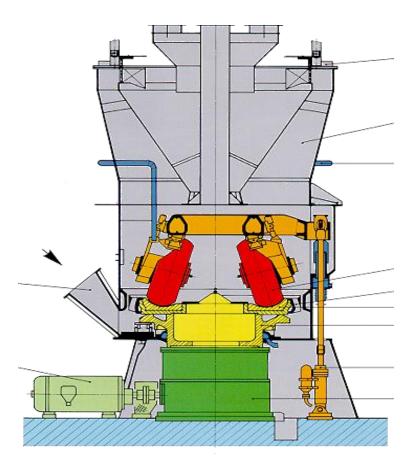
Types of pulverisers

Speed	Low 10 to 20 rpm	Medium 40 to 70 rpm	High 900 to 1000 rpm
Туре	Ball tube mills	Bowl Mill Ball & race Mill	Hammer mill, beater mill or fan mill
Dominating Principal	Attrition	Crushing	Impact



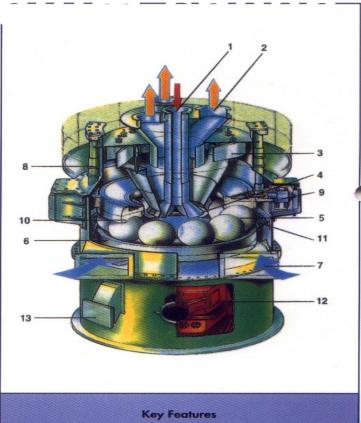
Tube mill





BOWL MILL

MPS MILL



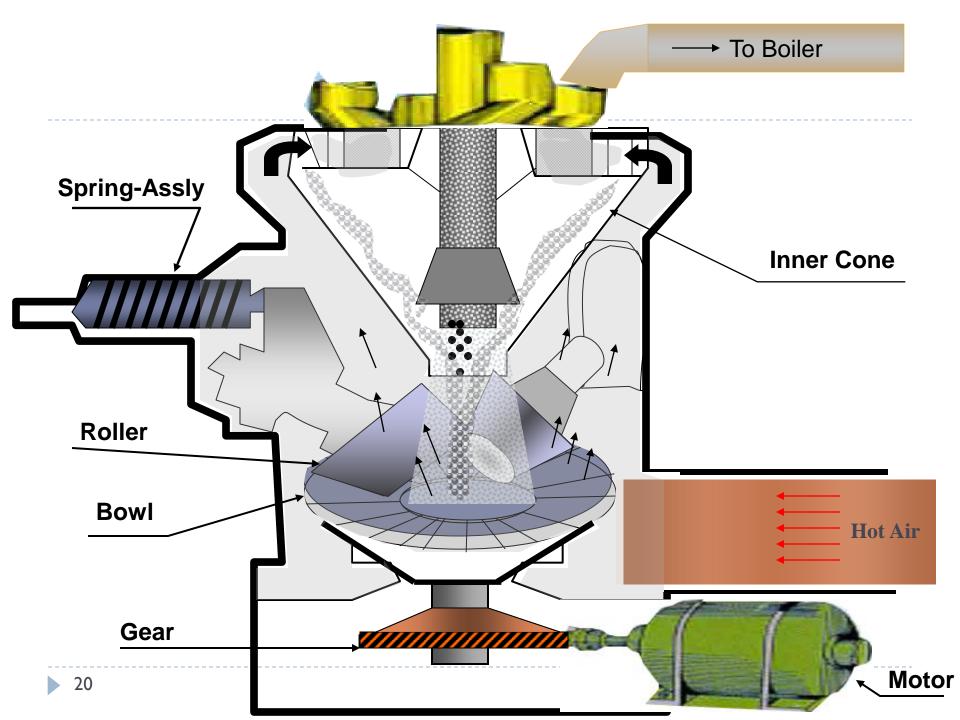
Raw Material Inlet

- 2 Product Outlet
- 3 Adjustable Classifier Blades
- 4 Oversize Particles Return Chute
- 5 Hollow Balls
- 6 Rotating Lower Grinding Ring
- 7 Primary Air Inlet

- 8 Loading Cylinders
- 9 Spider Guides
- 10 Stationary Upper Grinding Ring
- 11 Throat Plate
- 12 Gearbox
- 13 Reject Box

Ball & Race Mill

- 583 XRS / 803 XRP Bowl mills
- 58,80 stands for bowl diameter in inches
- If the number is even then its shallow bowl mill.
- If the number is odd then its deep bowl mill
- 3 number of rollers three nos.
 - X frequency of power supply 50 cycles. In USA 'x' means 60 cycles.
 - R- Raymond, name of the inventor
 - S- suction type with exhauster after mill
 - > P- pressurised type with P.A. Fan before mill.



Factors affecting Mill performance

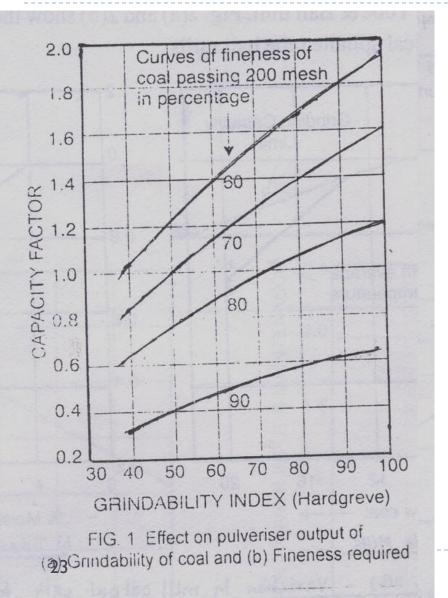
- Moisture in the coal.
- Coal grindability index.
- Mill inlet and outlet temp.
- Mill differential Pr. (DP)
- Mill loading.
- Air Flow in the Mill.
- Mill Motor current.
- Coal Mill fineness

- Grindability
- Moisture content
- Fineness
- Pri air quantity & temp

Effect of Grindability

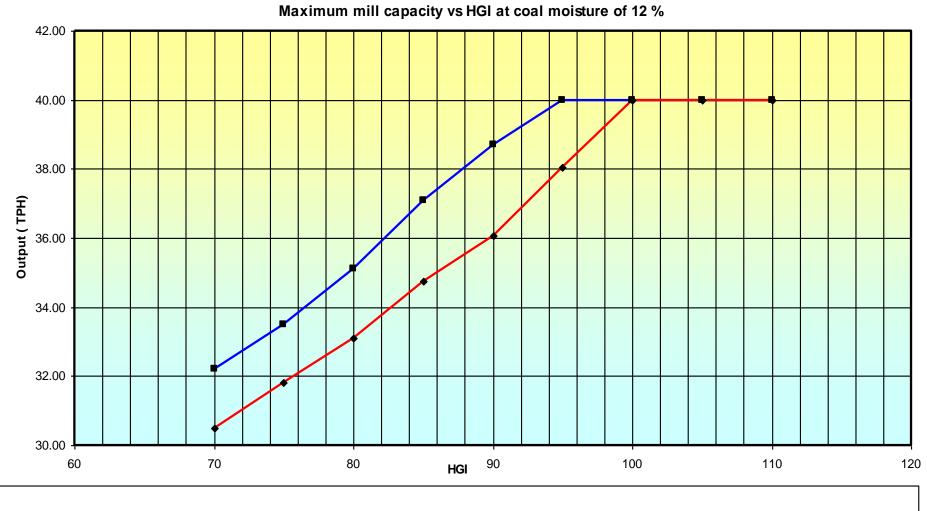
- The grind ability of the coal is an empirical index
- It is not an inherent property of coal
- Relative ease of grinding as compared with standard coal
- It is determined in laboratory using 50 g of air dried sample of properly sized coal in a miniature pulveriser which is set to rotate exactly 60 revolutions grinding the coal sample.
- The hard grove Gindablility index is calculated
 - G.I. (hardgrove) = 13+6.93W
 - Where W = weight of dust passing through 200 mesh sieve.

Effect of Grindability



- •Higher the HGI more is the capacity
- •Normally mill capacity is indicated at 50/55 HGI.
- Actual Mill capacity varies with HGI

Effect of Grindability



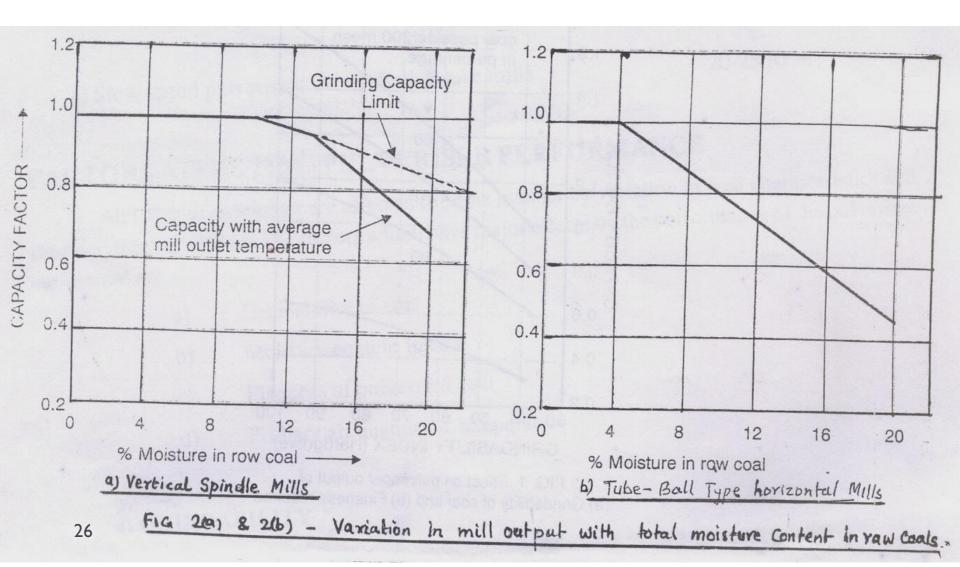
Output at coal fineness of 70 % passing through 200 Mesh

--- Output at coal fineness of 75 % passing through 200 mesh

Moisture in Coal

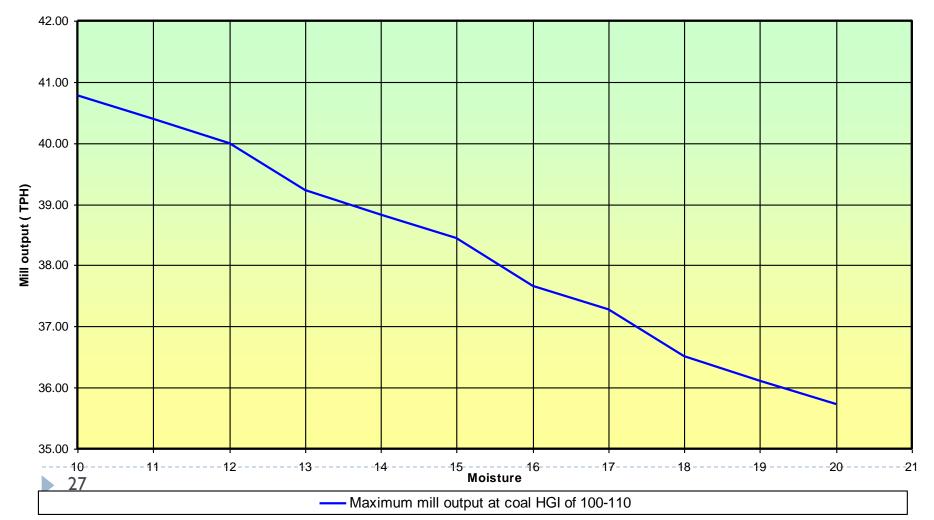
- Moisture: Inherent and surface
- Inherent moisture locked up within the structure
- Inherent moisture is constant for a particular seam
- Surface moisture varies
- Coal must be dried to remove the surface moisture totally before grinding
- Beside drying primary air also
 - Create circulation
 - Transport coal
 - Provide initial oxygen for combustion
- PA quantity is 15 to 28% of total air

Moisture in Coal



Effect of Moisture

Maximum mill Capacity vs coal moisture at coal HGI 100-110 and PF Fineness of 70 % passing through 200 Mesh



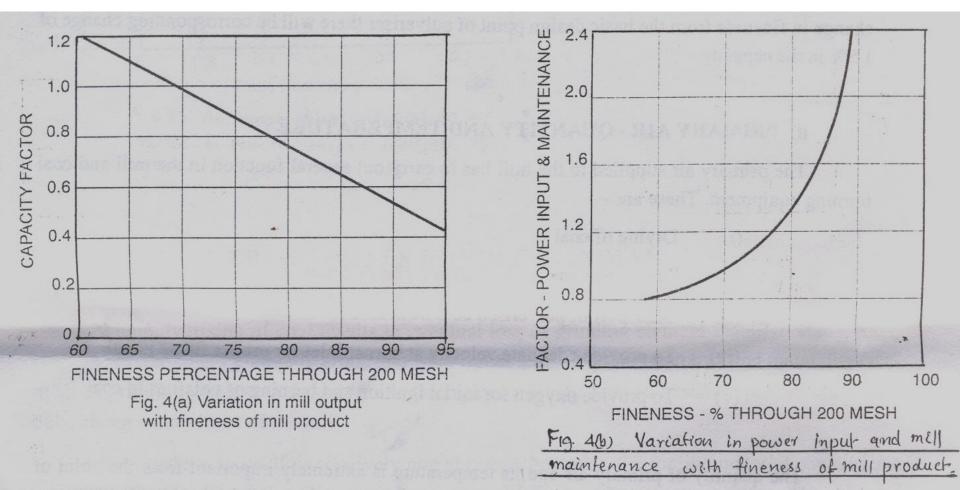
Temperature Of Coal –Air Mixture At Mill Outlet

- The temperature of pulverised coal and air mixture at pulveriser outlet should be maintained at least 15 °C Above the dew point of air at pulveriser pressure to avoid condensation and consequent plugging of the coal pipes.
- The pulveriser mill outlet temperature should be maintained above 65 °C.
- The higher limits are 90 °C For high volatile (above 24%) coals and 110 °C for low volatile coals (below20% VM)..

Effect of Fineness

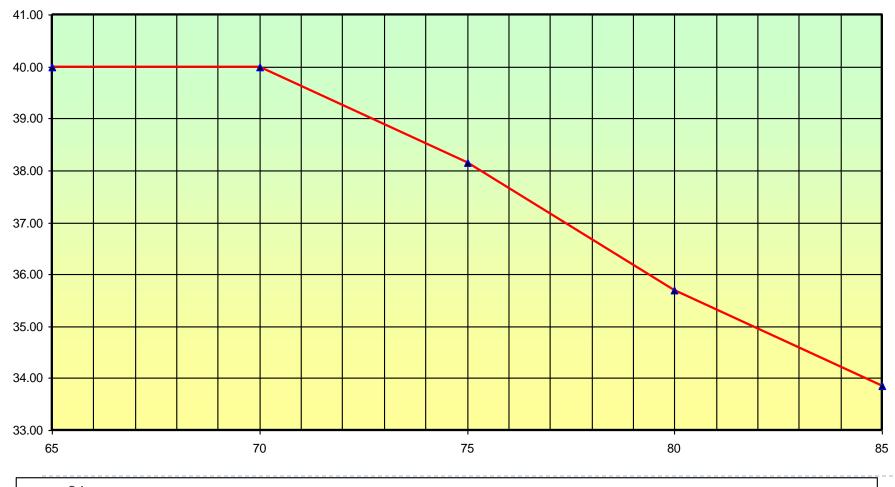
- Fineness of pulverised coal
- More the fineness less is the capacity
- > 70% through 200 mesh
- Number of opening per linear inch.
- 50 mesh sieve will have 2500 openings per square inch
- Volatile content below 16% would required higher degree of fineness i.E.75 to 80% through 200 mesh sieve, whereas the higher volatile coals (above 24%) will ignite and burn with ease with lower fineness of 60% through 200 mesh sieve.

Effect of Fineness



Effect of fineness

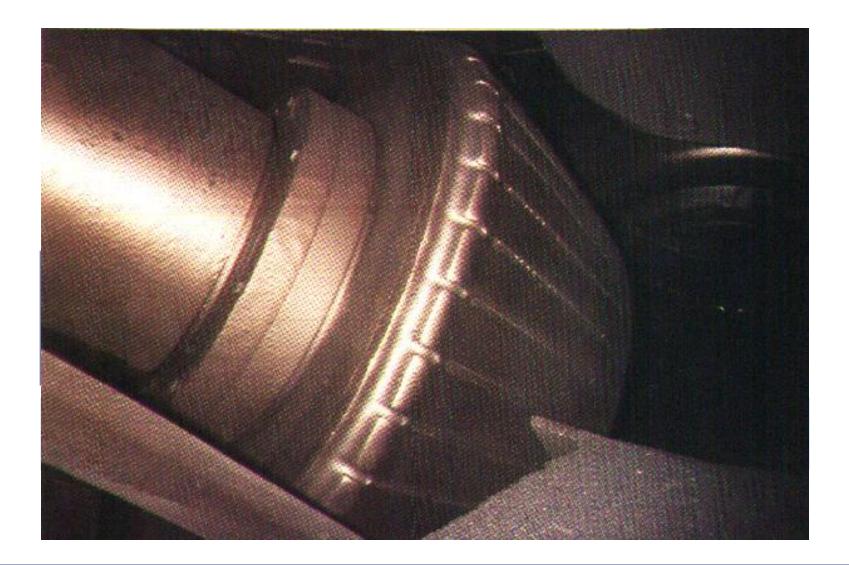
Maximum Mill capacity vs PF fineness at 12 % Raw coal moisture and at Coal HGI 100-110

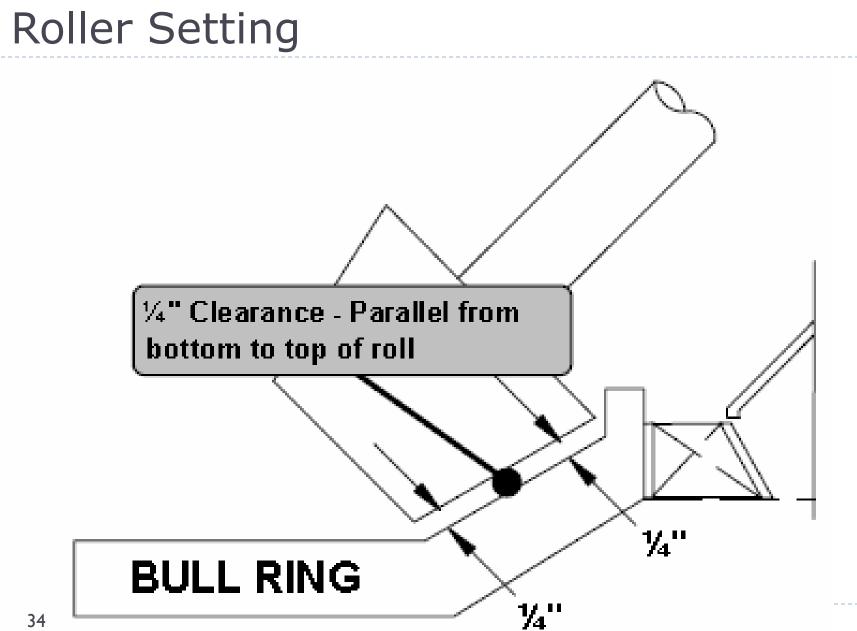


Fineness Requirement

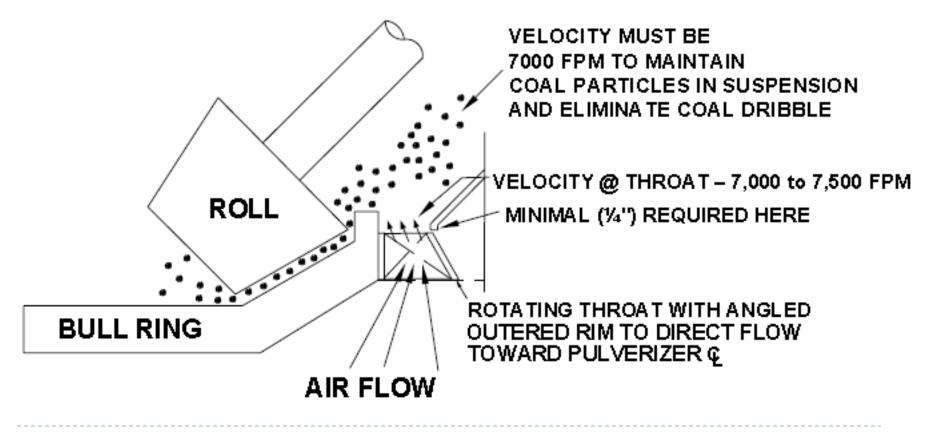
Sizing Range of Coals for PC Firing⁸⁰

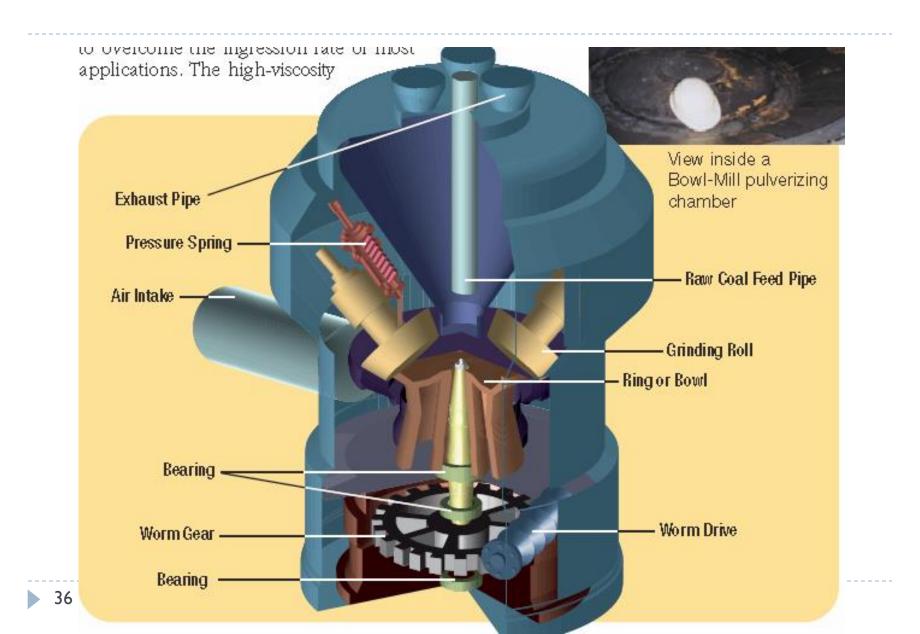
Coal rank	Passing 200 mesh, wt %	Retained on 50 mesh, wt %
Subbituminous C coal and lignite	60-70	2.0
High-volatile bituminous C, subbituminous A, B	65-72	2.0
Low- and medium-volatile bituminous C, high-volatile	70-75	2.0
bituminous A and B		



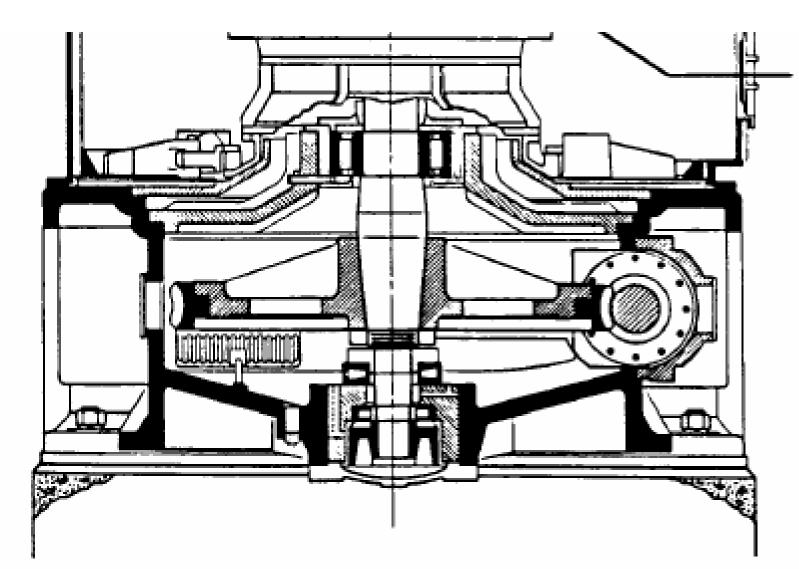


Throat Velocity

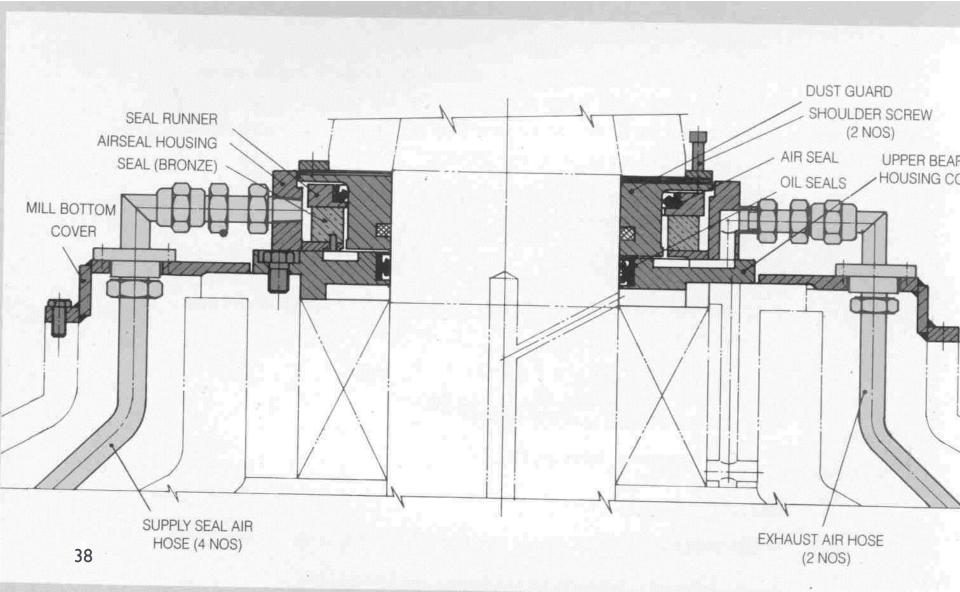




Mill Gear Box



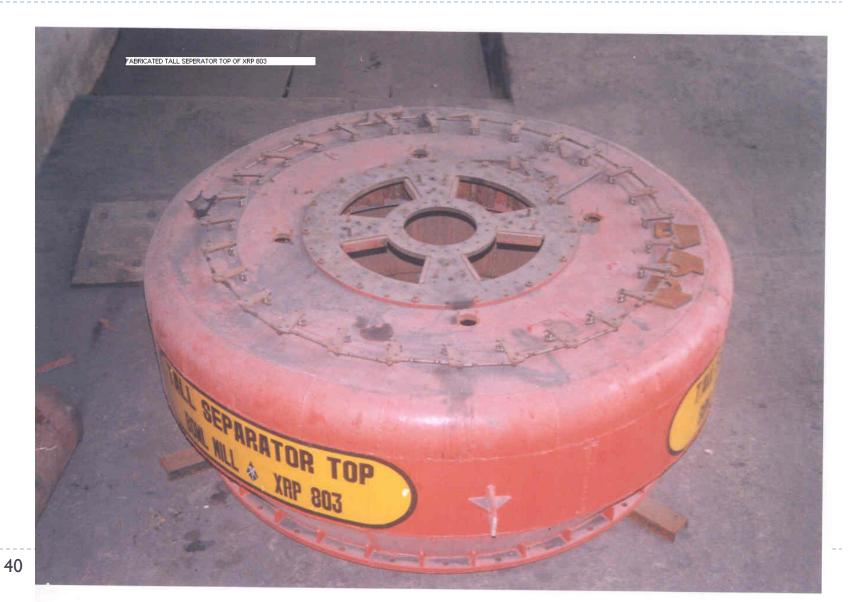
Mechanical face Seal



- Split type seals in journal and vertical Shaft
- Spring loaded mechanical face seal
- Ceramic tiles at separator body
- Tall separator top



Tall Separator Top



Tall Separator Top

Annexure -4

SEPARATOR TOP (TALL TYPE)



Split type seal

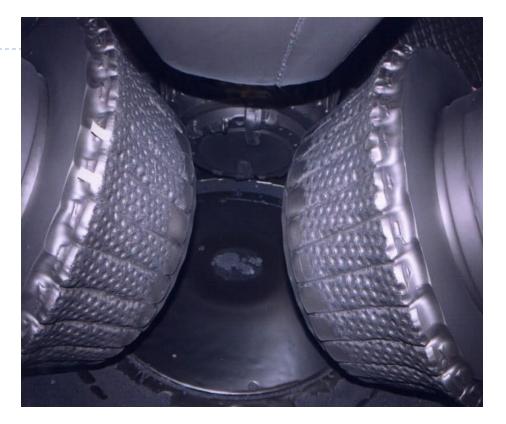


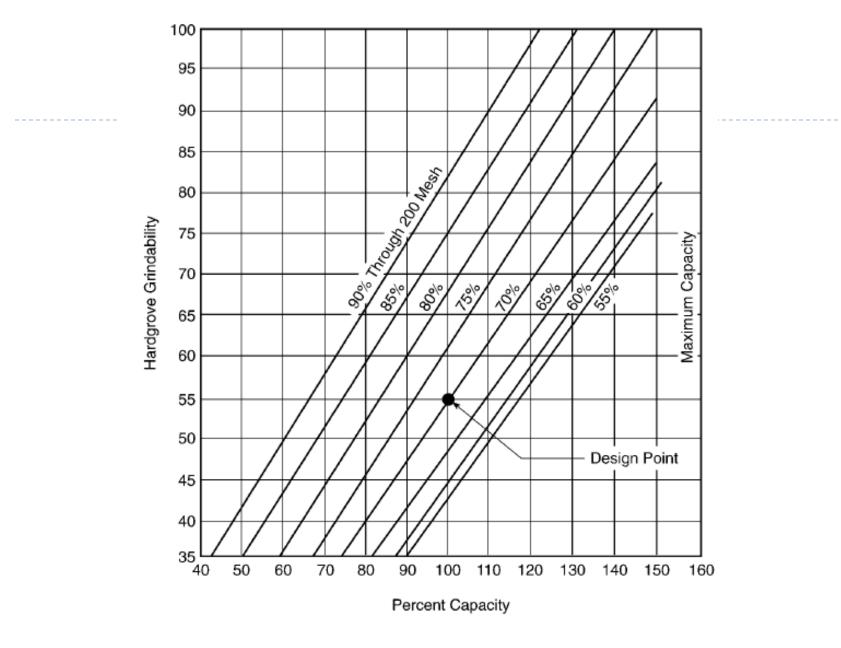
Effect Of Mill Internals On Mill Fineness

- Classifier blades opening
- Holes in classifier blades
- •Holes in innercone
- Improper gap between inverted cone and inner cone
- •Spring tension
- Clearance between grinding roll & brs
- •Wear out of grinding elements

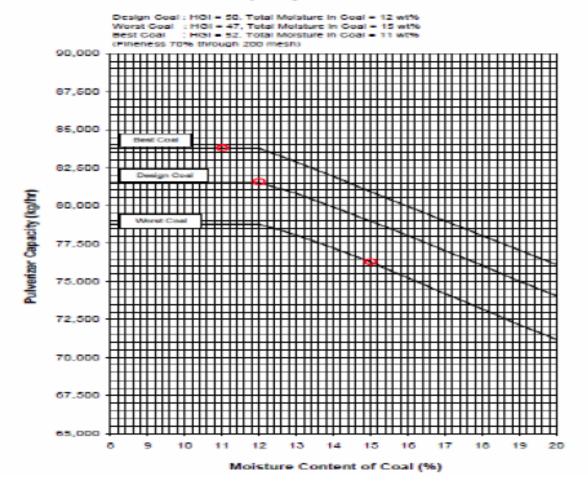
Factors Affecting Mill Performance

- HGI
- Fineness
- Moisture
- Size of raw coal
- Mill wear (YGP)
- Maintenance practices









Coal particle size distribution

- If 1-2% is +50 in BS mesh sieve (300 µm), most of this coarse coal will not burn and end up in C in BA
 - It also frequently causes slagging around the burners
 - If -200 mesh (75 µm) fineness is poor, results in high
 C in FA
 - If the coal is not properly ground, the distribution to the burners may not be even
 - Resulting in air-fuel imbalances at one or more burners

Fuel line balance

Mill discharge pipes offer different resistances to the flows

due to unequal lengths and different geometry/layouts.

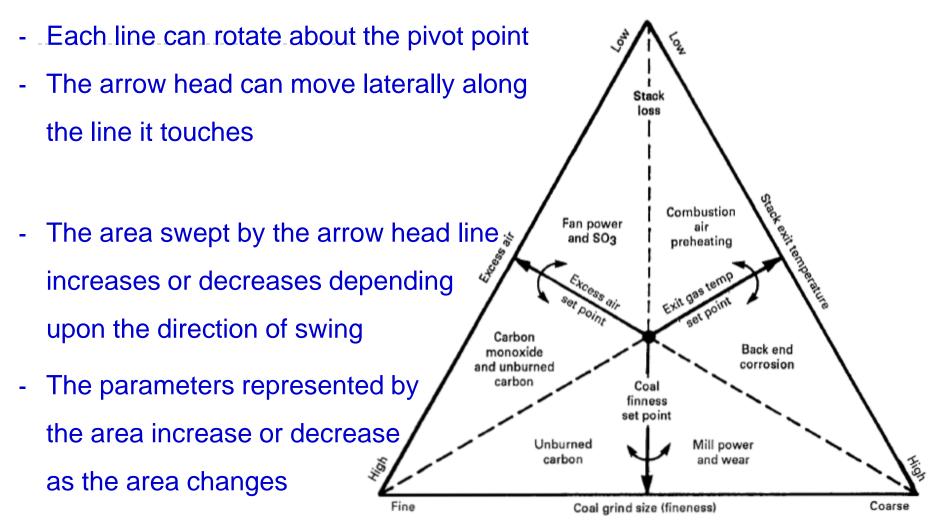
Fixed orifices are put in shorter pipes to balance velocities, dirty air / PF flows.

- > The sizes of the orifices are normally specified by equip. supplier
- Variable/adjustable orifices

Dirty air flow distribution should be within +/- 5%

Coal distribution within +/- 10% of the mean value

Interrelationship of parameters



Combustible in Ash Loss

Measure of effectiveness of Combustion process

and Mill performance

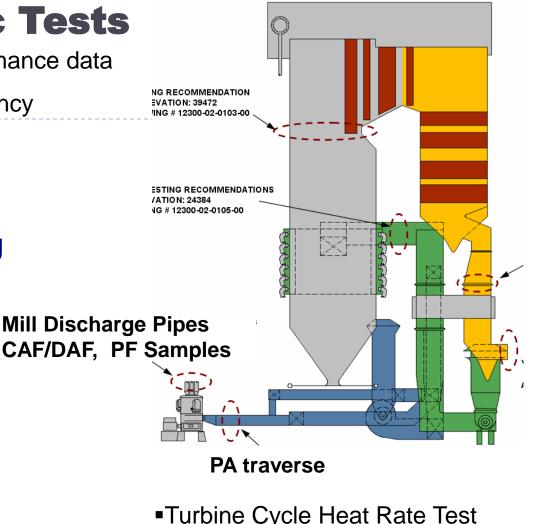
Loss in kJ/kg of fuel:

$$\frac{cA}{100}$$
 * 33820

- c= % of carbon in ash
- A= Mass of ash kg/kg of fuel
- Carbon burnt to $CO_2 = 33820 \text{ kJ/kg} (8077 \text{ kcal/kg})$
- Compute Boiler efficiency loss % due to c in Ash

The Diagnostic Tests

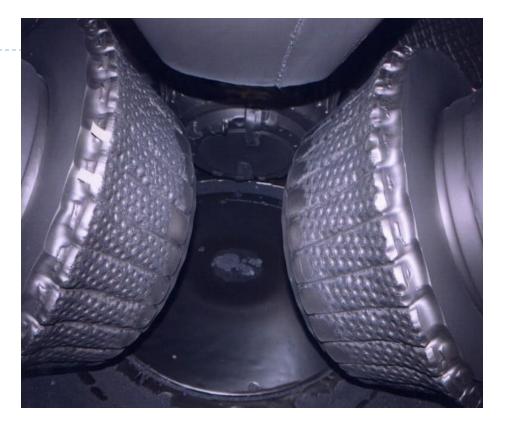
- Representative & accurate performance data
- RCA, Identify reasons for inefficiency
- Verify online FB
- **Dirty Airflow Tests**
- Iso-kinetic Coal Sampling
- PA Flow Calibration
- **Clean Airflow Tests**
- HVS
- Furnace Exit HVT
- Air In-Leakage survey
- Insulation survey
- Furnace temperature survey
- **Boiler Efficiency Tests**
- AH Performance Tests
 - Boiler Tuning & Optimization 51

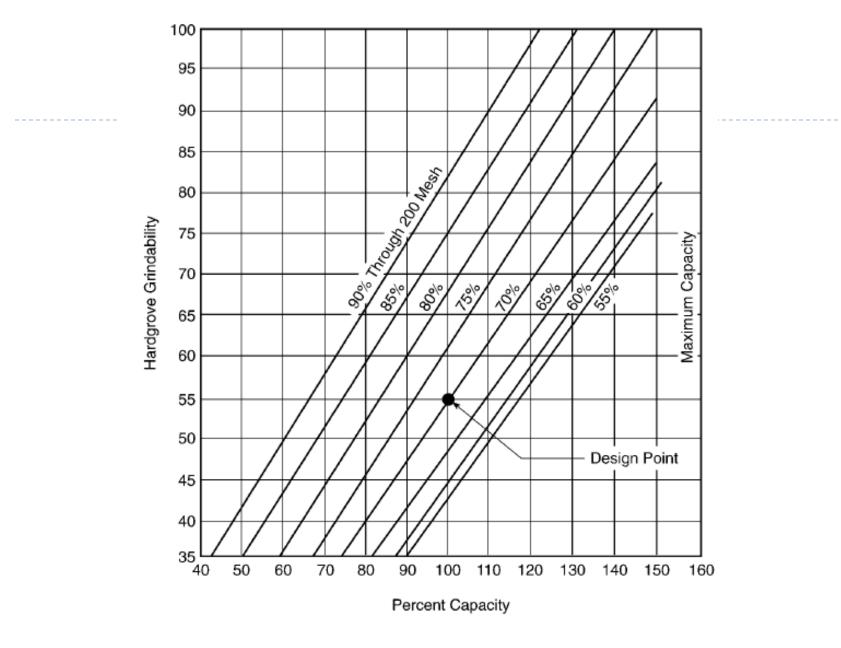


- Turbine Cycle Heat Rate Test
- Turbine Cylinder Efficiency Test
- Condenser Performance Test
- Condenser Air in-leak Test
- Heater Performance Test

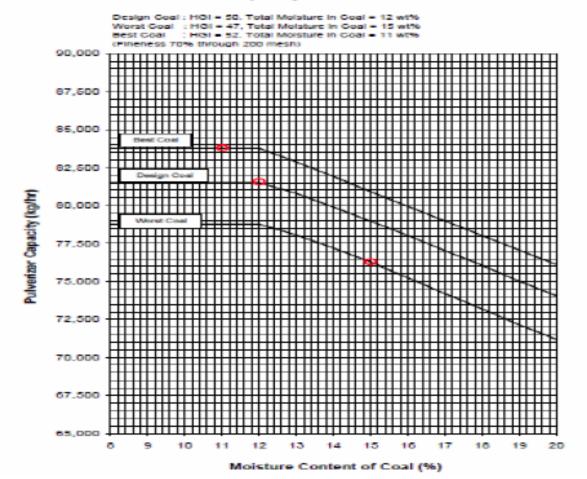
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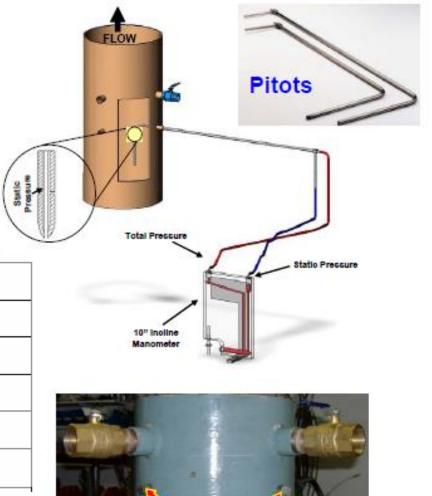
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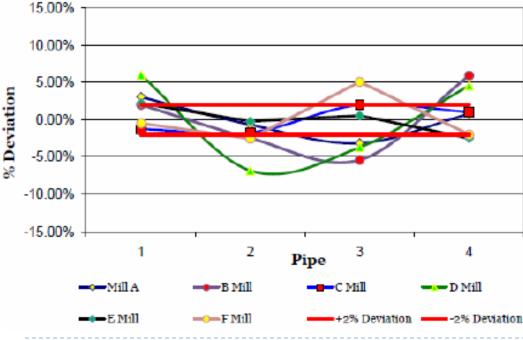
Coal distribution within +/- 10% of the mean value

Clean Air Flow Test

- Clean Air flowing through the fuel lines
 -at-normal-operating-temp and pres.
- Indicative of the transport energy
- Clean air vel. should be within +/- 2% of the mean.



Clean Air Test



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Dirty Air Flow Test

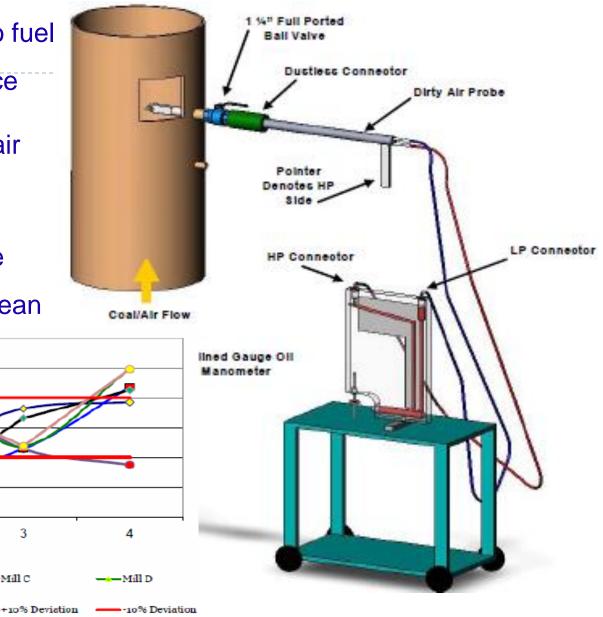
- PF air mix flowing thro fuel lines with mill in service
- To determine coal & air flow in each line
- Dirty air vel. should be within +/- 5% of the mean

2

-Mill B

-----Mill F

Pipe



→Mill A

−•−Mill E

1

30.00%

20.00%

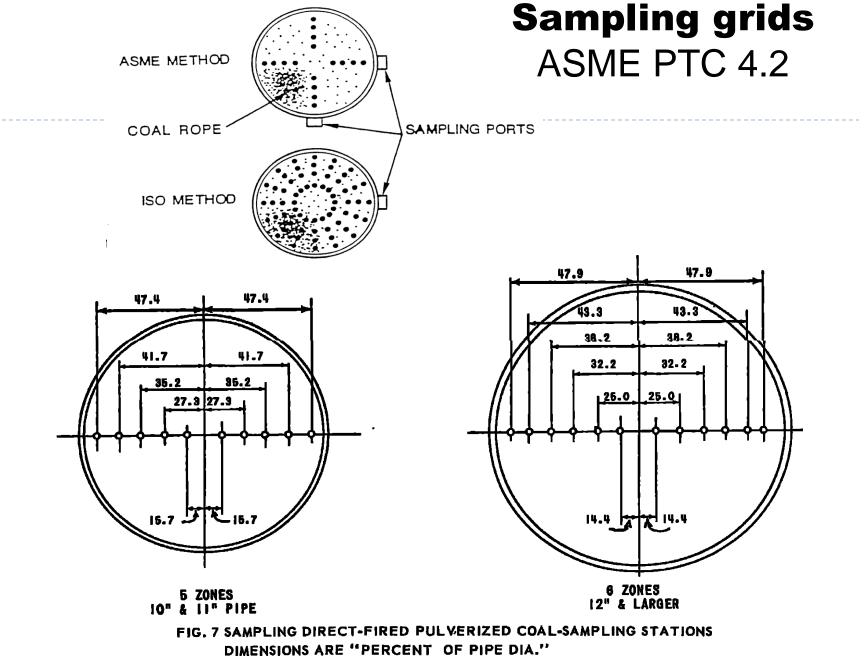
10.00%

0.00% Periation 0.00%

-20.00%

-30.00%

℅



Dirty Pitot Survey - Summary Data (Mill X)

	UCB	Measured
Air Flow T/hr	40	43.6
Mill Outlet Temp C	65	54.8
Coal Flow T/hr	-	26.2

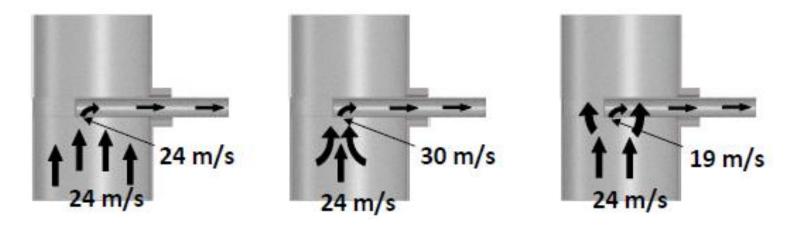
Description	Corner					
	1	2	3	4	Mean	Desired
Velocity m/s	24.3	22.9	16.0	17.4	20.2	> 18 m/sec
Air Flow T/hr	13.1	12.4	8.7	9.4	10.9	
Dev. From Mean %	20.2	13.8	-20.2	-13.8		< +/- 5%
Mill Out Temp ^o C	56.0	55.0	53.0	55.0	54.8	~ 85 °c
Coal Flow T/hr	7.9	5.8	5.6	6.9	6.6	< +/- 10%
A/F Ratio	1.7	2.1	1.0	1.4	1.6	1.8 to 2.5

Operating PA flow is lower by almost 4 - 5 T/h than design

- > Mill Outlet temperature is low in all the pipes.
- Low mill outlet temperature coupled with low PA flow could be the reason for the choking observed in Pipes 3 & 4.

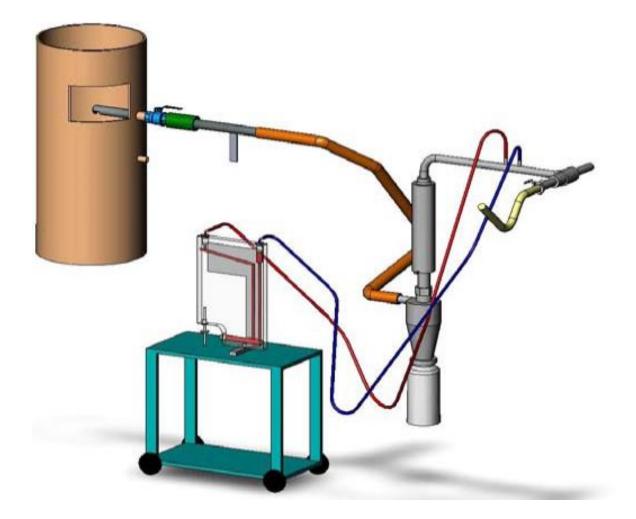
Iso-kinetic PF sampling

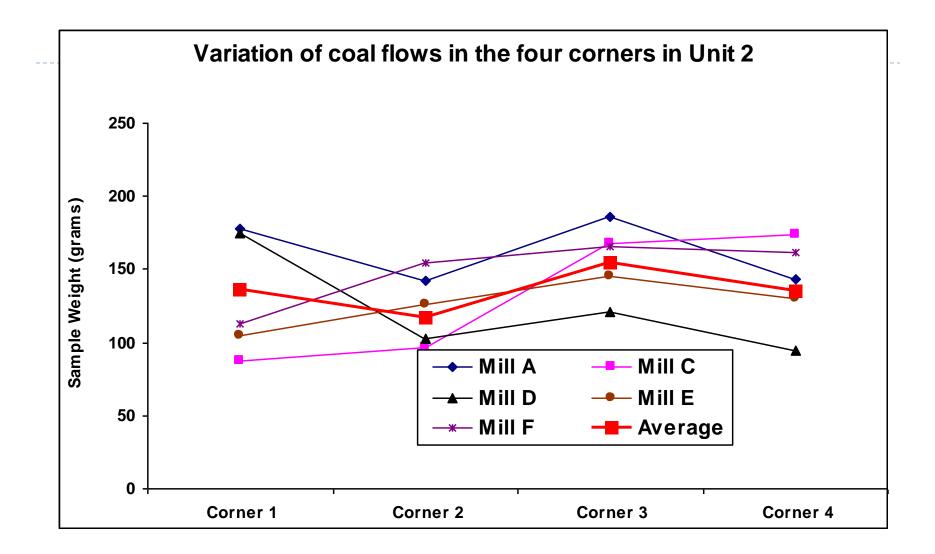
The velocity of dirty air entering the collection nozzle is equal to the velocity of the flow in the fuel line



More fines are drawn to the sampler

Allow fine particles to escape



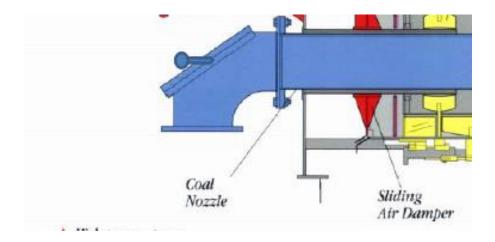


Case studies

Mill outlet temperature measurement
 Cold Junction Temp. Compensation Error

□ Temp. monitoring in each pipe

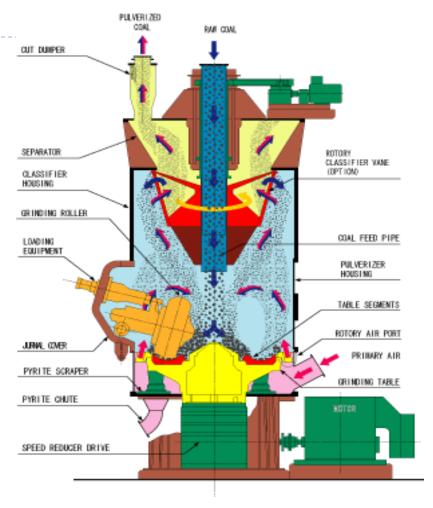
PF sampling point and sampling method



Case studies



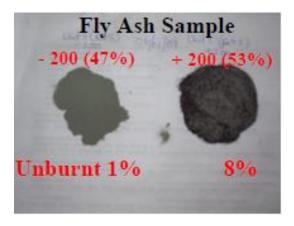
- Poor fineness in particular line
- Holes in classifier vanes
 - Poor fineness



High Unburnt in Fly Ash

Fineness or Air distribution problem?





PLACE 20 GRAMS OF ASH ON STACKED 200 MEASH AND PAN AND SHAKE FOR 20 MINUTES.

DETERMINE UNBURNT OF RESIDUE ON 200 MESH SCREEN AND IN PAN

Higher Unburnt in the pan indicates Air distribution problems while higher Unburnt in the sieve would indicate milling system problems In one case 53% of the ash retained on a 200 sieve was coarse & high in carbon (8%), while the -200 was soft, fluffy and had less unburnts (1%). This is indicative of poor fineness & problems in milling system.

Unburnt Carbon Loss (Controllable)

- C_{unburnt} is a measure of effectiveness of comb. process
- C_{unburnt} includes the unburned constituents in FA and BA
- +50 PF fineness fractions to be < 1%
- Focus to be on FA due to uncertainty in repeatability and representativeness





Flyash Canister Aspirator Sampling Tip Assembly Perforated Cylinder Flyash Extension for Filter Paper to Filter Pipe Canister Ball-Collect Flyash Sample Reducer Compressed Gas Air Flow.

FA sampling (HVS)

Factors - Unburnt C Loss

- Type of mills and firing system
- Furnace size
- PF fineness (Pulverizer problems)
- Coal FC/VM ratio, coal reactivity
- Insufficient excess air in combustion zone
- Air damper / register settings
- Burners design / condition
- Burner balance / worn orifices
- Primary Air Flow / Pressure



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